

# Windmill Palm Fiber/Polyvinyl Alcohol Nonwoven Fibrous Polymeric Materials

Changjie Chen<sup>1,2</sup>, Guicui Chen<sup>1,3</sup>, Guangxiang Sun<sup>1,2</sup>, Jiayi Wang<sup>4</sup>, Guohe Wang<sup>1,2</sup>

<sup>1</sup>College of Textile and Clothing Engineering, Soochow University, Suzhou, Jiangsu CHIINA

<sup>2</sup>Nantong Textile & Silk Industrial Technology Research Institute, Nantong, CHIINA

<sup>3</sup>Jiangsu Research and Development Center of the Ecological Textile Engineering and Technology, College of Textile and Clothing, Yancheng Institute of Industry Technology, Yancheng CHIINA

<sup>4</sup>China Filament Weaving Association, Beijing, CHIINA

Correspondence to:

Guohe Wang email: [wanguohe@suda.edu.cn](mailto:wanguohe@suda.edu.cn)

## ABSTRACT

Three types of wet-laid nonwoven materials with windmill palm fibril (WPF<sub>L</sub>), WPF<sub>L</sub>/windmill palm fiber bundles (WPFB) and windmill palm fiber (WPF)/polyvinyl alcohol (PVA), were prepared. The morphology and length distribution of WPF<sub>L</sub> and WPFB were analyzed by digital microscopy and image processing software. The filtration efficiency, air permeability and sound absorption properties of 12 samples of wet-laid nonwoven materials were tested. Adding PVA improved the porosity and enhanced the filtration efficiency, air permeability and acoustic properties of the nonwovens.

**Keywords:** Windmill palm fiber; PVA; Filtration efficiency; Air permeability; Sound absorption

## INTRODUCTION

Air pollution, a significant environmental problem, has attracted increasing attention due to rapid urbanization and industrialization [1]. In particular, particulates such as airborne bacteria and viruses are increasingly impacting the quality of life of the population [2-3]. Air pollution poses serious health threats to the public, and is a major cause of adverse health effects on the human respiratory tract, as well as a negative influence on climate and ecosystems [3-5]. Additionally, air pollution causes chemical corrosion and staining of fabrics, leather, metal products, construction materials and crops [6].

Among the many different groups of materials used for filter media, textile fabrics play an important role and are widely accepted [7]. In particular,

nonwoven fibrous filters made from cellulose produced by a wet-laid process (a modified paper-making process) are frequently used for air filtration applications [8,9]. Nonwovens are especially favored for filtration of sub-micron aerosols because of low production costs and wide ranging functionality[10]. The three-dimensional structure of nonwoven materials can not only improve filtration efficiency but can also increase the flow speed of the carrier phase, which can speed up the overall filtration process [11,12].

Palm fiber is an important lignocellulose fiber. Among the various types of palm fiber, oil palm fiber has been studied in depth is widely used as a reinforcing fiber in composites [13-16]. Though windmill palm is an abundant resource, research on its use as a filter is limited. It is well-documented that the smaller the fibers, the better the filtration performance of the fibrous filter [17]. The average diameter of the windmill palm fibril (WPF<sub>L</sub>) extracted from windmill palm is 10 μm [18], while the diameter of natural cotton fiber is 13~15 μm, ultrafine wool is 18~27 μm, ramie is 30~40 μm [19] and silk is 11~13 μm [20]. This indicates that WPF<sub>L</sub> is potentially one of the most suitable raw materials for filters.

The main objective of this research is to prepare a potential functional polymeric material based on cellulose that has good performance as a filter and also has good acoustic properties. To that end, three types of wet-laid nonwoven material with WPF<sub>L</sub>, WPF<sub>L</sub> / WPFB and WPF / PVA were prepared. The

filtration efficiency and air permeability of these samples were tested. The sound absorption properties of one type of WPF / PVA nonwoven material with high filtration efficiency and high air permeability was tested.

## **MATERIALS AND METHODS**

### **Preparation of Materials**

The windmill palm fiber used in this study was obtained from Mount Huang, Anhui Province, China. A portion of the fibers was treated with a solution of 4wt.% hydrogen peroxide ( $H_2O_2$ ) and 1.5 wt.% sodium hydroxide (NaOH) with a 1:50 fiber-to-extracting agent ratio (g/mL) at 90°C for 4 h. The residue was then filtered and put into a blender (Bm252c, Meidi, China) at 250 W and 20,000 r/min for approximately 30 s to obtain separated windmill palm fibril (WPF<sub>L</sub>). The other portion of the palm fibers was treated with a solution of 2 wt.%  $H_2O_2$  and 1 wt.% NaOH with an extracting ratio of 1:50 (g/mL) at 75°C for 3 h to obtain the WPFB, which were nearly free of lignin and hemi-cellulose. As a result, fine fiber with a small diameter can be obtained. More details about the sample preparation can be found in C. J. Chen et al [21]. The WPFB and WPF<sub>L</sub> were then washed with running water and dried in an oven with air circulation at 60°C for 24 hours.

### **Methods**

#### ***Preparation of Nonwoven Materials Based on WPF<sub>L</sub>***

Three types of nonwoven materials were prepared by means of a wet laid process. The first type was composed of WPF<sub>L</sub> only, with the amount of WPF<sub>L</sub> was increased from 10 g to 40 g in 10-g intervals to obtain samples with different thicknesses. These samples were denoted 1, 2, 3, and 4, respectively.

The second type was composed of WPF<sub>L</sub> and WPFB. The proportions of WPF<sub>L</sub> and WPFB were 80/20, 60/40 and 40/60. The total weight of fiber containing WPF<sub>L</sub> and WPFB for each sample was 40 g. These samples were denoted 5, 6, and 7.

The third type was composed of WPF<sub>L</sub> and WPFB (60/40, w/w), joined by PVA at concentrations of 0.1 wt.%, 0.5 wt.%, 1.0 wt.%, 1.5 wt.% and 2.0 wt. percent. The total weight of fiber containing WPF<sub>L</sub> and WPFB was 40 g. These samples were denoted 8, 9, 10, 11 and 12. For purpose of description, the material that contained WPF<sub>L</sub> and WPFB is called WPF throughout the remainder of this paper.

The wet laid process was used to prepare bamboo fiber, flax fiber and cotton nonwoven mats weighing 40 g. These three samples were denoted 13, 14 and 15, respectively.

WPF<sub>L</sub>, WPFB and 500 ml of deionized water or 500 ml of PVA with various concentrations were added to a blender. After blending, the compounded materials were formed into a mesh filter. The materials were then dried in an oven at 75°C.

#### ***Characterization of Windmill Palm Materials***

The morphologies of WPF<sub>L</sub> and WPFB were observed using a digital microscope (VHX-100, Keyence, Japan). Image processing software (Image-Pro Plus 5.0) was used to measure the diameter of WPF<sub>L</sub> and WPFB. More than 500 samples of each type of fiber were characterized.

#### ***Air Permeability Measurement***

The air permeability test was carried out on an air permeability testing apparatus (YG461E, Hongda, China). The air permeability was tested at a pressure differential of 100 Pa between the two surfaces of the nonwoven materials. Five different parts of each sample were tested, and the average was used as the air permeability.

#### ***Aerosol Filtration Efficiency Measurement***

The aerosol filtration efficiency was measured with an automated filtration testing unit (8130-1, TSI, America). NaCl aerosol particles of 260 nm average diameter and 75 nm count median diameter were prepared by an aerosol particle generator. Samples with an effective area of 100 cm<sup>2</sup> were tested at room temperature.

#### ***Sound Absorption Measurement***

The normal incidence absorption coefficient was measured by means of two microphone impedance tubes (SW463, Shengwang, China) using the transfer function method. The test specimens for testing were circular with an effective area of 100 cm<sup>2</sup> and 8.41 cm<sup>2</sup>. Samples were tested over frequency ranges from 60 Hz to 1.6 kHz and 1.6 kHz to 6.3 kHz.

## **RESULTS AND DISCUSSION**

### **Morphology and Diameter Distribution of WPF<sub>L</sub> and WPFB**

#### ***Morphology and Diameter Distribution of WPF<sub>L</sub>***

The average WPF<sub>L</sub> diameter and diameter distributions were characterized. A frequency

distribution diagram is commonly used for describing the diameter distribution. Origin 8.0 software was used to analyze these data, and the results are shown in *Figure 1*. The diameter distribution of WPF<sub>L</sub> is a normal distribution, with diameter between 8 and 14 μm in more than 90%, and the average diameter is 10.26 ± 2.1 μm. The minimum and maximum diameters of WPF<sub>L</sub> are 5.37 μm and 17.82 μm, respectively. The wide range of the diameter distribution creates a distribution of fabric pore sizes.

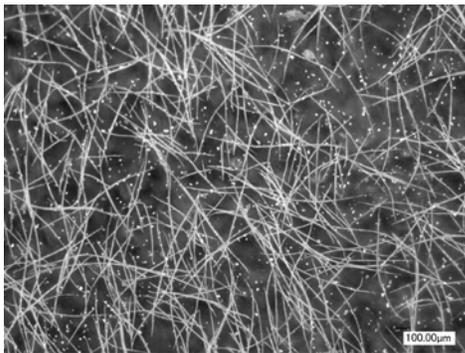
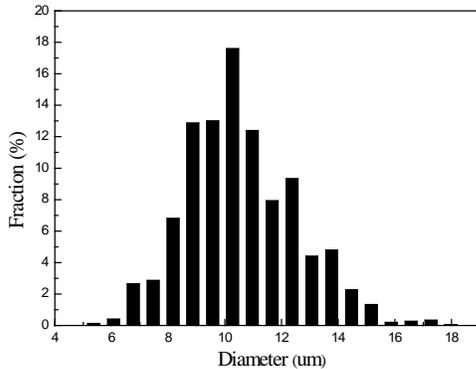


FIGURE 1. Morphology and diameter analysis of WPF<sub>L</sub>.

**Morphology and Length Distribution of WPF<sub>B</sub>**

The diameter of WPF<sub>B</sub> is shown in *Figure 2*, and it ranges from 40 μm to 290 μm. While the diameter distribution is nearly a normal distribution, fibers with a diameter between 70~170 μm comprise more than 90% of the total distribution. Additionally, the average diameter is 123.61±12.6 μm, which indicates that the diameter of WPF<sub>B</sub> is almost 10 times larger than that of WPF<sub>L</sub>, which takes the form of millimeter pores more easily. When combing these two types of materials to make nonwoven fabrics, a distribution of pores ranging from the micrometer to millimeter size is possible.

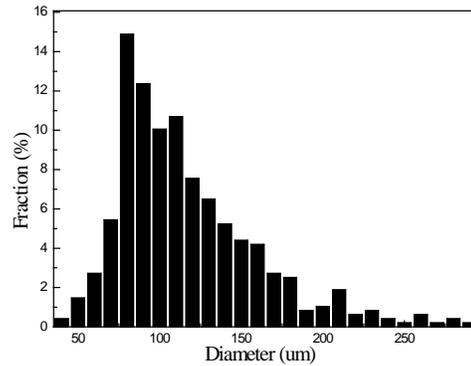
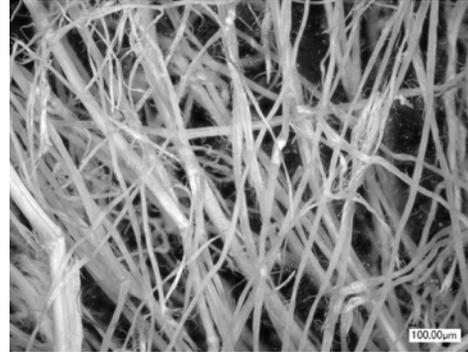


FIGURE 2. Morphology and diameter analysis of WPF<sub>B</sub>.

**Filtration Efficiency and Air Permeability of WPF<sub>L</sub> Nonwoven Materials**

As the amount of WPF<sub>L</sub> increases, the thickness of nonwoven materials increases, as illustrated in *Table 1*. The filtration efficiencies and air permeabilities of nonwoven materials with different amounts of WPF<sub>L</sub> are shown in *Figure 3*. The filtration efficiency increases as the thickness of nonwoven materials increases, and a linear correlation can be observed in *Figure 3a*. The R squared is 0.866, which indicates a good correlation. However, the air permeability decreases as the thickness of the nonwoven materials increases, and a linear correlation and a high R squared of 0.95 can be observed in *Figure 3b*. The interaction between filtration efficiency and air permeability is approximately a linear correlation, with an R squared of 0.75 as shown in *Figure 3c*.

Ideally a filter should have a combination of high filtration efficiency and high air permeability. However, the negative correlation between filtration efficiency and air permeability shown in *Figure 3c* means that an increase in the filtration efficiency will decrease the air permeability. Further results can be observed in *Figure 4*. When the filtration efficiency increases from  $45.15 \pm 2.19\%$  to  $67.40 \pm 1.05\%$ , then the air permeability decreases from  $137.55 \pm 7.08 \text{ mm}^3/\text{mm}^2\text{s}$  to  $72.47 \pm 5.67 \text{ mm}^3/\text{mm}^2\text{s}$ . Increasing the thickness to improve the filtration efficiency is not possible because the air permeability will become unacceptable. This relationship indicates that high filtration efficiency with high air permeability may not be possible for a material containing  $\text{WPF}_L$ .

TABLE I. Thickness of nonwoven materials with different amounts of  $\text{WPF}_L$ .

Samples	1	2	3	4
Areal density ( $\text{g}\cdot\text{m}^{-2}$ )	80	160	240	320
Thickness (mm)	2.07	3.81	7.31	10.26

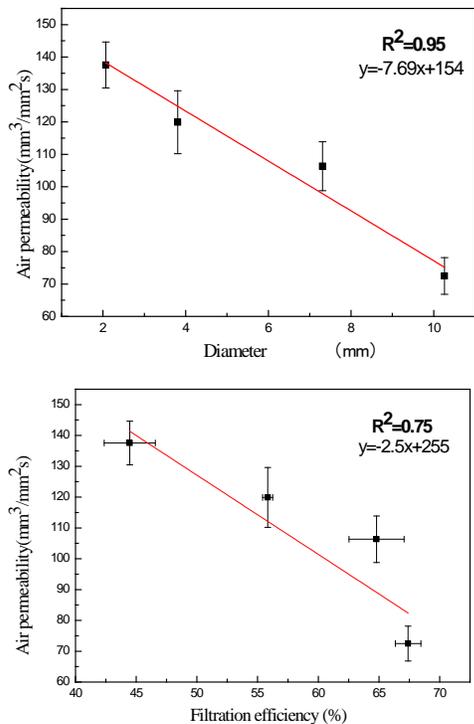


FIGURE 3. Correlation analysis among (a) diameter and filtration efficiency; (b) diameter and air permeability; (c) filtration efficiency and air permeability.

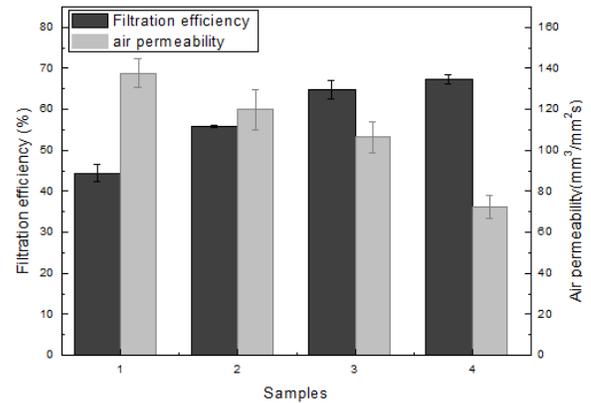


FIGURE 4. Filtration efficiency and air permeability of nonwoven materials with different amounts of  $\text{WPF}_L$ .

### Filtration Efficiency and Air Permeability of $\text{WPF}_L/\text{WPFB}$ Nonwoven Materials

$\text{WPFB}$  has a larger diameter than  $\text{WPF}_L$ , as shown in *Figure 1* and *Figure 2*. With increasing content of  $\text{WPFB}$ , more fibers with a diameter of approximately  $126.31 \mu\text{m}$  have been added into the nonwoven materials, and as a result, the air permeability increases. When the concentration of  $\text{WPFB}$  reaches 60 wt.%, the air permeability increases to the peak of approximately  $125.18 \pm 7.12 \text{ mm}^3/\text{mm}^2\text{s}$ . Filtration is a separation and purification process and filtration efficiency is one of the most critical measurements for filtration [22]. With the content of  $\text{WPFB}$  increasing from 0 wt.% to 40 wt.%, the filtration efficiency increases. However, when the content of  $\text{WPFB}$  is above 40 wt.%, a clear decline can be observed in *Figure 5*. The highest filtration efficiency is  $77.17 \pm 2.06\%$ , while the air permeability is  $88.22 \pm 4.97 \text{ mm}^3/\text{mm}^2\text{s}$ .

Increasing fiber diameter decreases the filtration efficiency because due to decreased particle impact probability resulting from a lower number of fibers [23,24]. The  $\text{WPFB}$  with a large diameter can increase the fiber surface roughness, which can improve the particle collection efficiency due to the presence of asperities [25]. The fibrillation of  $\text{WPFB}$  during the alkali treatment not only increases the surface asperities but also increases the micro pores, which can filter small particles. These characteristics all have a positive effect on the filtration efficiency. However, increasing the level of large diameter  $\text{WPFB}$  in nonwovens can increase the macro pores and the particles may go through the materials freely. As a result, the

filtration efficiency will decrease. This effect is evident from *Figure 5* as filtration efficiency is observed to decrease in Sample 7, where the WPFB level reaches 40 percent.

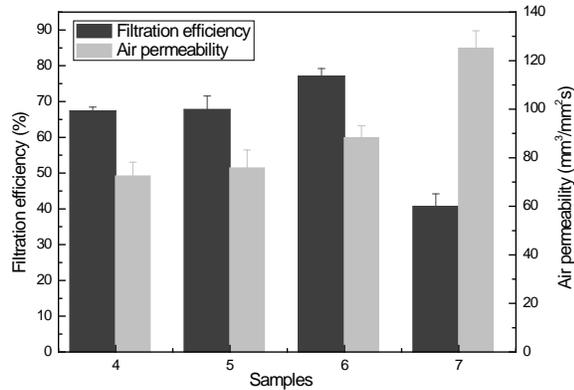


FIGURE 5 Filtration efficiency and air permeability of nonwoven materials with different WPFB contents.

#### Filtration Efficiency and Air Permeability of WPF / PVA Nonwoven Materials

The filtration efficiency and air permeability of nonwoven materials with different concentrations of PVA are shown in *Figure 6*. As the concentration of PVA increases from 0.1 wt.% to 1.0 wt.%, the filtration efficiency and air permeability increase. The film-forming tendencies of PVA in conjunction with mechanical blending produce many bubbles during the process of wet laying [26]. After drying, some of the bubbles remain, effectively increasing the porosity and improving the filtration efficiency and air permeability. As PVA concentration increases, it becomes more difficult for the PVA to form bubbles, which causes the number of pores in the materials decrease. As a result, a decrease in the filtration efficiency is observed when the PVA concentration becomes greater than 1.5 wt. percent. However, when PVA concentration increases above 1.0 wt.%, a film forms on the surface. As PVA concentration increases further, a more and more complete film is formed. Hence, a decrease in the air permeability is observed. The highest filtration efficiency is  $88.87 \pm 1.75\%$ , with an air permeability is  $92.18 \pm 3.59 \text{ mm}^3/\text{mm}^2\text{s}$ . The filtration efficiencies of the bamboo fiber nonwoven mat of sample 13, flax fiber mat of sample 14 and cotton mat of sample 15 are  $63.90 \pm 2.13\%$ ,  $61.41 \pm 1.68$  and  $67.80 \pm 0.96\%$  respectively, much lower than those of WPF / PVA nonwoven materials.

Meanwhile, the air permeabilities of the three mats are more than  $120 \text{ mm}^3/\text{mm}^2\text{s}$ , significantly higher than that of WPF / PVA.

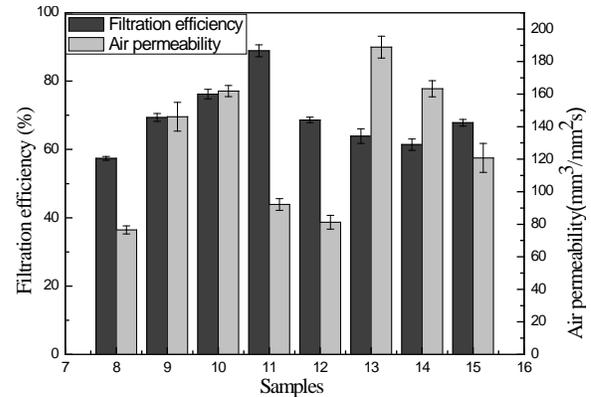


FIGURE 6. Filtration efficiency and air permeability of nonwoven materials with different concentrations of PVA.

#### Sound Absorption Properties of WPF / PVA Nonwoven Material

As shown in *Figure 7*, the WPF / PVA nonwoven material with an areal density of  $320 \text{ g/m}^2$  does not absorb sound because the sound absorption coefficient was below 0.2 at the frequency range of 80 to 800 Hz. With increasing frequency, the sound absorption coefficient increases initially and reaches a peak of approximately 0.95 at a frequency of 4000 Hz. This increase with frequency has been observed by others. For example, a 16.38-mm thick commercial glass fiber needle-punched mat [27] and a 12-mm thick nature luffa fiber mat [28] reach peaks of 0.62 and 0.6 respectively, both at a frequency of 6300 Hz. However, further increases in the frequency led to a slight decrease in the sound absorption properties. This result indicates that WPF / PVA nonwoven material has better sound absorption properties than do glass fiber and luffa fiber. The average sound absorption coefficient of sample 11, at 12-mm thick, is calculated by averaging the absorption coefficients at frequencies of 250, 500, 1000, 2000, and 4000 Hz, and the result is approximately 0.36. Meanwhile, the sound absorption coefficient of 20-mm thick kapok fibrous material is approximately 0.24 [29].

Factories in most cases face both air particle and multi-frequency noise pollution. The WPF / PVA nonwoven material exhibits good combination of particle filtration and noise absorption properties

and is attractive from the standpoint of sustainability being cellulose based. The material should be of high interest in industrial environments where such combinations of particle and noise reduction are required.

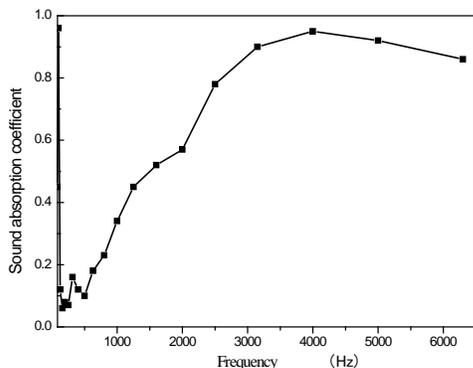


FIGURE 7. Sound absorption coefficient of WPF / PVA nonwoven materials.

## CONCLUSION

Different diameters of WPF<sub>L</sub> and WPF<sub>B</sub> and polymeric material PVA were used to prepare tree types of nonwoven materials. The average diameter of WPF<sub>L</sub> is  $10.26 \pm 2.1 \mu\text{m}$ , with a distribution from  $5.37 \mu\text{m}$  to  $17.82 \mu\text{m}$ . Meanwhile, the average diameter of WPF<sub>B</sub> is  $123.61 \pm 12.6 \mu\text{m}$ , with a distribution from  $40 \mu\text{m}$  to  $290 \mu\text{m}$ . Increasing the level the larger WPF<sub>B</sub> fibers increases the air permeability of the resulting nonwovens, and increases filtration efficiency until the loading reaches 40%, at which point filtration efficiency begins to decrease.. When the content of WPF<sub>B</sub> reaches 40 wt.%, the highest filtration efficiency of  $77.17 \pm 2.06\%$  achieved, while the air permeability is  $88.22 \pm 4.97 \text{ mm}^3/\text{mm}^2\text{s}$ . The material with 1.5 wt. % PVA has the best balance of properties, with filtration efficiency at  $88.87 \pm 1.75\%$ , air permeability is  $92.18 \pm 3.59 \text{ mm}^3/\text{mm}^2\text{s}$ , and an average sound absorption coefficient of approximately 0.36.

## ACKNOWLEDGMENT

This work was funded by the Priority Academic Program Development of Jiangsu Higher Education Institutions, China (No.37 [2014]); Nantong Technological Innovation Project, China (No.XA2012006); and Jiangsu Province Special Project, China (No.BY2014083).

## REFERENCES

- [1] W. Na, A. Raza, S. Yang, J. Yu, S. Gang, and B. Ding, "Tortuously structured polyvinyl chloride/polyurethane fibrous membranes for high-efficiency fine particulate filtration," *Journal of Colloid & Interface Science*, vol. 19, no. 398, pp. 240-246, 2013.
- [2] Y. Li, K. Xiao, J. Luo, J. Lee, S. Pan, and K. S. Lam, "A novel size-tunable nanocarrier system for targeted anticancer drug delivery," *Journal of Controlled Release*, vol. 3, no. 144, pp. 314-323, 2010.
- [3] H. Luo, B. Jiang, B. Li, Z. Li, B. H. Jiang and Y. C. Chen, "Kaempferol nanoparticles achieve strong and selective inhibition of ovarian cancer cell viability," *International journal of nanomedicine*, no. 7, pp. 3951, 2012.
- [4] B. Liu, S. Zhang, X. Wang, J. Yu, and Ding, B, "Efficient and reusable polyamide-56 nanofiber/nets membrane with bimodal structures for air filtration," *Journal of colloid and interface science*, no. 457, pp. 203-211, 2015.
- [5] E. S. Lee, C. C. D. Fung, and Y. Zhu, "Evaluation of a High Efficiency Cabin Air (HECA) Filtration System for Reducing Particulate Pollutants Inside School Buses," *Environmental science & technology*, vol. 6, no.49, pp. 3358-3365, 2015.
- [6] C. K. Liu and J. W. Ma, "Development and Application of Nonwovens Filter Materials," *Qingdao University Textile and Garment College*, vol. 13, no. 1, pp. 30-34, 2005.
- [7] K. B. Im and Y. K. Hong, "Development of a melt-blown nonwoven filter for medical masks by hydro charging," *Textile Science & Engineering*, vol. 4, no. 54, pp. 186-192, 2014.
- [8] J. D. Spengler, and Q. Chen, "Indoor air quality factors in designing a healthy building," *Annual Review of Energy and the Environment*, vol. 1, no. 25, pp. 567-600, 2000.

- [9] R. Agnes, B. Marc, L. C. Laurence, M. Evelyne, S. Albert and L. C. Pierre, "Combined air treatment: Effect of composition of fibrous filters on toluene adsorption and particle filtration efficiency," *Chemical Engineering Research & Design*, no. 86, pp. 577-584, 2008.
- [10] J. Payen, P. Vroman, M. Lewandowski, A. Perwuelz, S. Calle-Chazelet and D. Thomas, "Influence of fiber diameter, fiber combinations and solid volume fraction on air filtration properties in nonwovens," *Textile Research Journal*, no. 82, pp. 1948-1959, 2012.
- [11] K. Thangadurai, G. Thilagavathi and A. Bhattacharyya, "Characterization of needle-punched nonwoven fabrics for industrial air filter application," *The Journal of The Textile Institute*, vol. 12, no. 105, pp. 1319-1326, 2014.
- [12] C. C. Eng, N. A. Ibrahim, N. Zainuddin, H. Ariffin, M. Z. W. Y. Wan, and Y. Y. Then, "Enhancement of mechanical and dynamic mechanical properties of hydrophilic nanoclay reinforced polylactic acid/polycaprolactone/oil palm mesocarp fiber hybrid composites," *International Journal of Polymer Science*, vol. 20, no. 10, pp. 3679-3684, 2014.
- [13] Y. Y. Then, N. A. Ibrahim, N. Zainuddin, H. Ariffin, and M. Z. W. Y. Wan, "Oil palm mesocarp fiber as new lignocellulosic material for fabrication of polymer/fiber biocomposites," *International Journal of Polymer Science*, vol. 4, pp. 1-7, 2013.
- [14] B. X. Ni and P. Zhang, Study on pore size distribution and filtration efficiency of nonwovens, *Industrial textiles*, vol. 258, no. 3, pp. 25-27, 2012.
- [15] S. Shinoj, R. Visvanathan, S. Panigrahi and M. Kochubabu, "Oil palm fiber (OPF) and its composites: A review," *Industrial Crops and Products*, no. 33, pp. 7-22, 2011.
- [16] N. Izani, M. T. Paridah, and U Anwar, "Effects of fiber treatment on morphology, tensile and thermogravimetric analysis of oil palm empty fruit bunches fibers," *Composites Part B Engineering*, vol. 1, no. 45, pp. 1251-1257, 2013.
- [17] H. Ma, B. S. Hsiao and B. Chun, "Thin-film nanofibrous composite membranes containing cellulose or chitin barrier layers fabricated by ionic liquids," *Polymer*, vol. 12, no. 52, pp. 2594-2599, 2011.
- [18] C. J. Chen, Y. Zhang, G. H. Wang, "Structure and Properties of Medical Hollow Palm Sheath Fibril," *Journal of Donghua University(English Edition)*, vol. 31, no. 5, pp. 617-620, 2014.
- [19] M. Yao, "Textile materials science" [M]. Beijing: China textile publishing house, 2009.
- [20] Y. X. Zhang, Textile materials science [M]. Beijing: China textile publishing house, 2010.
- [21] C. J. Chen, Y. Zhang, G. X. Sun, J.Y. Zhang, and G. H. Wang, "Morphology Research of Windmill Palm (*Trachycarpus fortunei*) Material," *Kemija u industriji*, vol. 9-10, no. 64, pp. 467-472, 2015.
- [22] M. E. Yuksekkaya, M. Tercan, and G. Dogan, "An experimental investigation of nonwoven filter cloth with and without reinforcement of woven fabric," *The Journal of the Textile Institute*, vol. 11, no. 101, pp. 950-957, 2010.
- [23] C. B. Song, and H. S. Park, "Analytic solutions for filtration of polydisperse aerosols in fibrous filter," *Powder Technology*, vol. 2, no. 170, pp. 64-70, 2006.
- [24] J. Steffens, and J. R. Coury, "Collection efficiency of fiber filters operating on the removal of nano-sized aerosol particles: homogeneous fibers," *Separation & Purification Technology*, vol. 1, no. 58, pp. 99-105, 2007.
- [25] G. E. R. Lamb, P. Costanza and B. Miller, "Influences of fiber geometry on the performance of nonwoven air filters," *Textile Research Journal*, vol. 45, no. 45, pp. 452-463, 1975.
- [26] C. C. DeMerlis and D. R. Schoneker, "Review of the oral toxicity of polyvinyl alcohol (PVA)," *Food and Chemical Toxicology*, vol. 3, no. 41, pp. 319-326, 2003.
- [27] M. Kucuk and Y. Korkmaz, "Sound absorption properties of bilayered nonwoven composites," *Fibers and Polymers*, vol.4, no. 16, PP. 941-948, 2015.

- [28] H. Koruk and G. Genc, "Investigation of the acoustic properties of bio luffa fiber and composite materials," *Materials Letters*, no. 157, PP. 166-168, 2015.
- [29] H. Xiang, D. Wang and H. Liua, "Investigation on sound absorption properties of kapok fibers," *Chinese Journal of Polymer Science*, vol.5, no. 31, PP. 521-529, 2013.

#### **AUTHORS' ADDRESSES**

**Changjie Chen**

**Guicui Chen**

**Guangxiang Sun**

**Guohe Wang**

College Of Textile and Clothing Engineering

Soochow University

Renai Road 199

Suzhou, JiangSu 314500

CHIINA

**Jiayi Wang**

China Filament Weaving Association

Beijing

CHIINA